Adiabatic Quantum Motors Raul Bùstos-Marun, Gil Refael, and Felix von Oppen PRL 111, 060802 (2013)

In 1960 Richard Feynamm announced a contest and promised a \$1000 prize to the developer of an engine that fits a cube of side 1/64" (~0.4 mm)

Introduction

Motor: device capable of converting energy into movement





kinetic energy -> rotational motion

electric energy-> rotational motion

"As the dimensions of motors are reduced, it is natural to expect that quantum mechanics could be used to operate and to optimize nanomotors"

Quantum motors and quantum pumps

The main idea is to use the same operating principle as an electron pump, but in reverse

Chaotic QD pump

Thouless pump





The motor (wheel) changes the shape of the QD

The conveyor belt generates a time-periodic potential felt by the electrons



Electrons are pumped through the device

Quantum motors and quantum pumps

Chaotic QD pump

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The voltage V induced a motion of the electrons that induce a force on the (classical) mechanical degree of freedom θ

The problem is treated within scattering theory formalism



Here assume that the scattering matrix depends on several (classical) mechanical motor degrees of freedom X_{ν}

$$S = S(\mathbf{X})$$

Force exerted on mechanical degree of freedom [PRL 107, 036804 (2011)]

$$F_{\nu}(\mathbf{X}) = \sum_{\alpha} \int \frac{d\epsilon}{2\pi i} f_{\alpha} \operatorname{Tr}\left(\prod_{\alpha} S^{\dagger} \frac{\partial S}{\partial X_{\nu}}\right) \qquad \text{Projects onto scattering}$$

channel in lead α

lpha=L,R ϵ : electron energy $f_{lpha}(\epsilon)$: Fermi distribution in lead lpha

Output Power $F_{\nu}(\mathbf{X}) = \sum_{\alpha} \int \frac{d\epsilon}{2\pi i} f_{\alpha} \operatorname{Tr}\left(\Pi_{\alpha} S^{\dagger} \frac{\partial S}{\partial X_{\nu}}\right)$

For nonzero voltage V, the force F is NOT conservative

$$W_{\rm out} = \oint d\mathbf{X} \cdot \mathbf{F}(\mathbf{X}) \neq \mathbf{0}$$

In linear response
$$W_{\text{out}} = \frac{ieV}{4\pi} \oint d\mathbf{X} \cdot \int d\epsilon f'(\epsilon) \operatorname{Tr} \left[(\Pi_L - \Pi_R) S^{\dagger} \frac{\partial S}{\partial \mathbf{X}} \right]$$

This is proportional to the pumped charge into the system [PRB **58**, R10135 (1998)]
 $\longrightarrow W_{\text{out}} = Q_p V$ and $P_{\text{out}} = Q_p V / \tau$

Efficiency

The input power is given by the standard expression

 $P_{\rm in} = \bar{I}V$

current induced by the voltage V

The efficiency of the motor is naturally defined as

$$\eta = P_{\rm out}/P_{\rm in} = Q_p/\bar{I}\tau$$

Define G(x) as the conductance of the device

$$\longrightarrow \quad \overline{I} = \overline{G(\mathbf{X})}V + \frac{Q_p}{\tau}$$

$$\rightarrow \quad \eta = \frac{1}{1 + \bar{G}V\tau/Q_p}$$

Relation between the efficiency and the pumped charge!

QD pump is purely quantum mechanical effect

----> Quantum motor

Thouless pump

Efficieny 1 for Fermi energy below the gap

Motor Dynamics

Assume the (classical) mechanical degree of freedom is subject to damping γ

$$\gamma \dot{\theta} = \frac{Q_p V}{2\pi} - F_{\text{load}}$$

Cycle period of the motor $\tau=2\pi/|\dot{ heta}|=(2\pi)^2\gamma/(Q_pV-2\pi F_{
m load})$

Use
$$\bar{I} = \overline{G(\mathbf{X})}V + \frac{Q_p}{\tau} \longrightarrow \frac{1}{\tau} = \frac{Q_p\bar{I} - 2\pi F_{\text{load}}\bar{G}}{Q_p^2 + (2\pi)^2\gamma\bar{G}}$$

Thouless motor with conductance G=0 $\longrightarrow 1/\tau = \overline{I}/Q_p$

current is solely due to pumped charge

maximal load

 $F_{\rm load}^{\rm max} = Q_p \bar{I}/2\pi G$

Thouless motor

Let us investigate the Thouless motor in more detail



$$\mathcal{H} = p^2/2m + 2\Delta \cos(2\pi x/a + \theta)\Theta(L/2 - |x|)$$
Periodic chemical potential

Choose Fermi wavevector close to $k_0 = \pi/a$

 $\begin{array}{l} \longrightarrow \\ \mbox{Hamiltonian can be linearlized} \\ \mathcal{H} = v_F p \sigma^z + \Delta (\sigma^x \cos\theta + \sigma^y \sin\theta) \Theta (L/2 - |x|) \\ \mbox{act in space of counterpropagating channels} \\ \end{array}$

A formula for the scattering matrix can then be determined

$$S = \frac{1}{M_{11}} \begin{pmatrix} -ie^{i\theta} \frac{\Delta}{\sqrt{E^2 - \Delta^2}} \sin\lambda_L & 1\\ 1 & -ie^{-i\theta} \frac{\Delta}{\sqrt{E^2 - \Delta^2}} \sin\lambda_L \end{pmatrix} \begin{pmatrix} \lambda_L = (L/\hbar v_F) [E^2 - \Delta^2]^{1/2} \\ M_{11} = \\ \cos\lambda_L - i(E/\sqrt{E^2 - \Delta^2}) \sin\lambda_L \end{pmatrix}$$

Thouless motor

From the expression for the scattering matrix, we determine the conductance (Landauer)

$$G = \bar{G} = \frac{e^2}{h} \frac{|\Delta^2 - E_F^2|}{|\Delta^2 - E_F^2|\cos^2\lambda_L + E_F^2|\sin\lambda_L|^2}$$

From Brouwer's formula at zero temperature for an angular mechanical degree of freedom [PRB 58, R10135 (1998)] we obtained the pumped charge

$$Q_p = \frac{e\Delta^2 |\sin\lambda_L|^2}{|\Delta^2 - E_F^2|\cos^2\lambda_L + E_F^2|\sin\lambda_L|^2}$$

and thus the efficieny

$$\eta = \frac{1}{1 + \frac{2\pi\gamma}{\hbar} \frac{|E_F^2 - \Delta^2|}{\Delta^4 |\sin\lambda_L|^4} [|E_F^2 - \Delta^2|\cos^2\lambda_L + E_F^2|\sin\lambda_L|^2]}$$



Conclusions